

voestalpine Böhler Welding

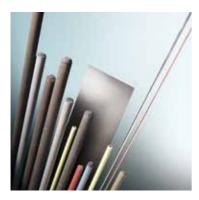




voestalpine Böhler Welding

Metallurgical Expertise for Best Welding Results

voestalpine Böhler Welding (formerly Böhler Welding Group) is a leading manufacturer and worldwide supplier of filler metals for industrial welding and brazing applications. With more than 100 years of experience, the enterprise has decisively influenced the development of welding technology, setting the benchmark with its innovative solutions. The solidity is also reflected in the confidence of our employees who, as owners of the enterprise, hold a good portion of the shares.



As a part of the voestalpine Group, Austria's largest steel manufacturer and one of the world's leading suppliers of specialized steel products, we are a part of a global network of metallurgy experts.

Our customers benefit from:

- Comprehensive welding and steel know-how under one roof
- Coordinated complete solutions comprised of steel and welding filler metals
- A partner offering maximum economic stability and technological expertise

Customer first

Absolute customer focus is our guiding principle. We see ourselves as a provider of solutions to challenging welding projects. We ensure that our customers get the right filler metals, use them correctly, and that all welding process parameters are adjusted for the best possible performance. We consider it as our responsibility to guarantee that we deliver to our customers, now and in the future, the best possible solutions. We also strive to develop new products, optimize existing products, and streamline processes so as to achieve very short turnaround times.

Experienced and committed employees

We rely on committed employees who have been trained to the highest standards. It is their knowledge, skills, and personal commitment that ensure the long-term success of our company and its customers. In combination with our premium quality products, the individual technical support provided by our globally acting application technicians and specialist welding engineers empowers our customers to master even the most difficult and challenging welding tasks.



Three competencies - three brands

In our efforts to afford our customers the best possible support and promote development in line with specific targets, we have built our core competences within Joint Welding, Repair & Maintenance Welding and Soldering & Brazing. This way we offer our customers the largest and most comprehensive product portfolio of filler materials within our three brands:

- Böhler Welding
- UTP Maintenance
- Fontargen Brazing

Welding Solutions for demanding industries

We focus on industries with high technological standards and deliver products tailored to industry-

specific requirements. In the development and optimization of filler materials, we collaborate closely with customers, manufacturers, and research institutes.

Whether destined for use in challenging scenarios or in standard applications – our high quality filler materials are ideally suited for all applications in the following industry sectors:

- Oil and Gas
- Pipeline
- Chemical
- Power Generation
- Transportation & Automotive
- Maintenance & Repair
- Brazing Industries

Our Industry Competence Comes From Experienced People

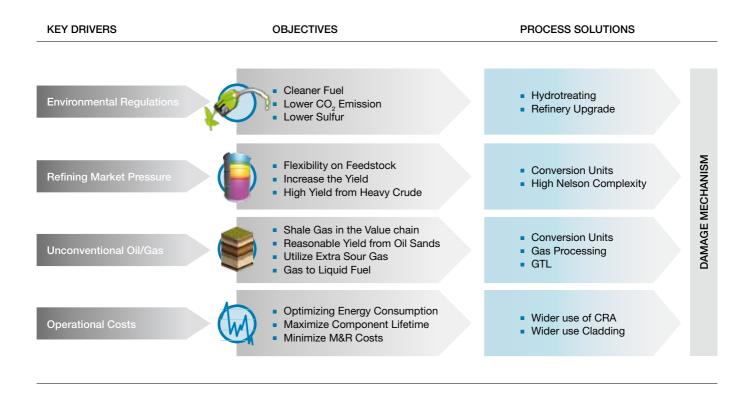
Oil and gas play an important role in the future global energy supply model. However, the emergence of new and unconventional sources of oil and gas will change the landscape with regard to extraction and processing in many significant ways. Upstream Oil & Gas refers to the search for crude oil and natural gas, followed by their recovery and production. This segment is also referred to as the Exploration and Production (E&P) sector; it includes the search for potential underground or sub-sea oil and gas fields, the drilling of exploratory wells, and the subsequent drilling and operation of the wells that recover and bring the crude oil and/or raw natural gas to the surface. Downstream Oil & Gas refers to the refining and processing of the extracted oil and gas from both conventional and unconventional resources. This segment is also referred to as hydrocarbon processing and includes refineries, natural gas processing plants, Olefins and Aromatics as well as Methanol plants.



voestalpine Böhler Welding provides solutions driven by its high-quality welding consumables for safe, efficient, and cost-effective operation of upstream, midstream, and downstream facilities and equipment to these segments worldwide. These products are supplied by regional manufacturing, development, sales, and support units under a range of products that are recognized worldwide.

Oil & Gas Downstream – Walking on the Edge of Steel Limits

Global demand for fuel products is increasing. The quality of petroleum compounds, such as crude oil or natural gas that is extracted in different geographical locations varies, and extra-heavy oil is playing a more significant role than in the past. More sources of unconventional oil and gas from oil sands and shale have been recently explored, and they have been receiving a great deal of attention. Today, environmental regulations with regard to fuels and petrochemical products have become more stringent.

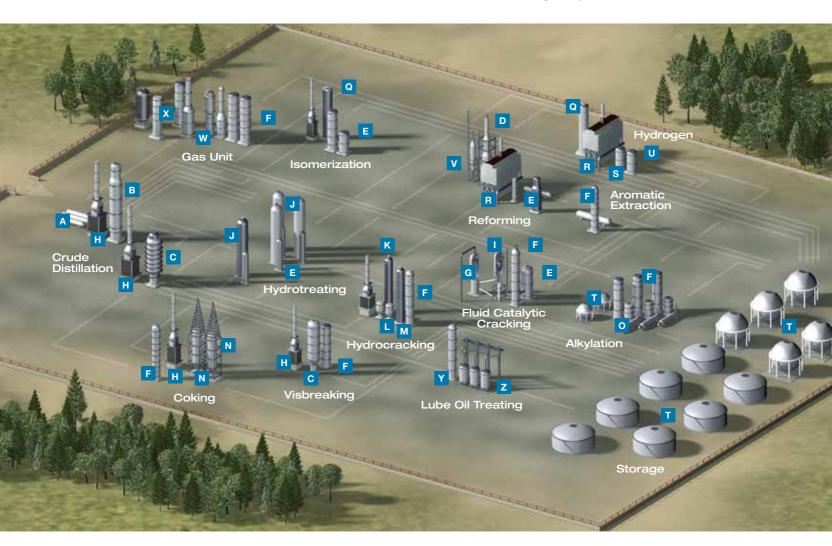


All these variables put together a complicated function in front of the oil and gas "super-majors" to make top-quality products especially from extra-heavy feedstock, and still achieve a healthy margin. As shown in this road map derived from the key drivers, the main challenge in setting defined objectives and developing solutions is to maintain the integrity of the process component while dealing with a wide range of damage mechanisms. These additional damage mechanisms are either related to the unconventional feedstock or enhanced service conditions.

In recent years, steel manufacturers have been developing better steel grades to withstand such service conditions. One must take into consideration that steel products need to be welded or cladded by weldoverlay; it is at this point that customers face the main welding challenges. A good example is development of vanadium-enhanced Cr-Mo steels, which require special weld fabrication expertise. Welding consumables may seem to be a very small part of this industry, but almost all oil and gas downstream experts confirm that welding and welding technologies are the main drivers in the development of optimized process reactors and furnaces. The requirements for welding consumables in the downstream segment are generally considered to be more stringent than the conventional standard requirements for the same grades in other fields. In the following, we will summarize the most important damage mechanisms in each of the three main plants. We will also be providing information about two of the major challenges: fabrication of hydroprocessing reactors (Page 8) and reforming / cracking furnaces (Page 13).

Oil Refineries

Hydrocarbon molecules come in many different sizes and shapes that generally depend on the quality of the crude oil. In an oil refinery, five different process categories are utilized to achieve both a higher yield and cleaner fuel.



- Fractionating hydrocarbon molecules by size, e.g., in a crude distillation unit
- Cracking larger molecules into smaller ones, e.g., in a fluid catalytic cracking unit or a hydrocracking unit
- **Combining** smaller hydrocarbon molecules into larger molecules, e.g., in an alkylation unit
- Changing the molecule shapes, e.g., in a catalytic reforming unit
- Hydrotreating units are also needed to reduce sulfur, aromatics, nitrogen, oxygen, and metals while enhancing the combustion quality, density, and smoke point of fuels

Depending on the process, its feedstock and operating conditions, various damage mechanisms can pose a threat to the life cycle of a refinery, to equipment integrity, and to plant safety. Many of these damage mechanisms can directly or indirectly relate the quality of welding consumables and welding condition. Some of the major damage mechanisms are listed in this text.

The choices regarding the base material used for critical process equipment in a refinery as well as for weld-overlay cladding are limited. Some of these choices are listed in Table A, which refers directly to the relevant product for the target grade.

Unit	Damage Mechanisms
Crude	Sulfidation
Distillation Unit	Wet H2S Damage (Blistering/HIC/SOHIC/SCC)
	Creep / Stress Rupture
	Polythionic Acid Stress Corrosion
	Naphetanic Acid Corrosion
	Ammonium Chloride Corrosion
	HCI Corrosion
	Caustic Corrosion / Cracking
	Erosion / Erosion-Corrosion
	Aqueous Organic Acid Corrosion
	Fuel Ash Corrosion
Gas Unit	Sulfidation
	Wet H2S Damage (Blistering/HIC/SOHIC/SCC)
	Ammonium Bisulfid Corrosion
	Chloride SCC
	Flue Gas Dew Point Corrosion
	Amine Corrosion / Cracking
	Titanium Hybriding
	Sulfuric Acid Corrosion
Isomeriza- tion Unit	High Temperature Hydrogen Attack (HTHA)
	HCI Corrosion
	Caustic Corrosion / Cracking

Table B: Damage mechanisms

			Joining Alloy Choices									Wel	d-O	verl	ay C)epc	osit	Cho	ices													
	Components	C-Mn	C- ½ Mo	1 1/4 Cr 1/2 Mo	2 ¼ Cr 1 Mo	2 ¼ Cr 1 Mo ¼ V	5 Cr ½ Mo	9 Cr 1 Mo	S.S 304H	S.S 310	Alloy 800 / 800H	Alloy HP / HP Nb	S.S 347	Alloy 600	Alloy 625	Alloy 825	Alloy 617	1% Ni	2.5% Ni	3% Ni	S.S 410S	S.S 308L	S.S 308H	S.S 316L	S.S 317L	S.S 347	Alloy 254 SMo	Alloy 276	Alloy 825	Alloy 625	Alloy 400	Alloy 200
Α	Desalter	•																				•					•		•	•		
В	Atmospheric Distillation Tower	•																			•			•	•							
С	Vacuum Distillation Tower	•																														
D	Naphtha Reformer Reactor			•																												
E	Feed/Effluent Heat Exchanger		•	•	•	•																•		•		•					•	•
F	Fractionator	•		•																	•	•		•							•	•
G	FCC Regenerator	•	•																				•									
н	Fired Heater								•	•																						
1	FCC Reactor				•	•															•											
J	HDS Reactor	•			•	•																				•						
K	Hydrocracking Reactor				•	•																				•						
L	Hot Separator				•																					•						
М	Cold Separator	•																						•								
Ν	Coke Drum			•																	•									•		
0	Alkylation Reactor	•																											•	•	•	•
Р	Post Heater/Furnace Piping						•	•	•	•			•																			
Q	Hydrogenation Reactor			•	•												•									•						
R	Steam Reformer Furnace										•	•																				
S	Low Temp. Shift Convertor	•																														
т	Storage Tanks	•																•	•	٠												
U	High Temp. Shift Convertor			•																												
V	CCR Regenerator		•								•	•																				
w	Sulfur Recovery Piping													٠	•	•																
X	Sour Water Stripper	•																										•				
Υ	Extraction Tower	•																			•			•	•							
Ζ	Evaporator	•							•	•																						

Table A: Alloy choices for major refinery components

Unit	Damage Mechanisms	Unit	Damage Mechanisms	Unit	Damage Mechanisms
Delayed	Sulfidation	Vis-	Sulfidation	Catalytic	High Temperature Hydrogen Attack
Coking	Wet H2S Damage	breaking	Wet H2S Damage	Reforming	HCI Corrosion
	(Blistering/HIC/SOHIC/SCC)		(Blistering/HIC/SOHIC/SCC)		Creep / Stress Rupture
	Creep / Stress Rupture		Polythionic Acid Corrosion		Temper Embrittlment
	Naphetanic Acid Corrosion		Naphetanic Acid Corrosion		Carburization
	Ammonium Chloride Corrosion		Ammonium		Hydrogen Embrittlement
	Ammonium Bisulfide Corrosion		Ammonium Chloride Corrosion		Ammonia SCC
	Thermal Fatigue		Ammonium Bisulfide Corrosion		Mechanical Fatigue
	Carburizaion		Carburization		Metal Dusting
	Dealloying		Chloride SCC	Lube Oil	Phenol (Cabolic Acid) Corrosion
	Carbonate SCC		Creep / Stress Rupture	Alkylation	Caustic Corrosion / Cracking
Hydro-	Sulfidation		Sour Water Corrosion		HF Acid Corrosion
treating &	Wet H2S Damage	FCCU	Sulfidation		Erosion / Erosion-Corrosion
Hydro-	(Blistering/HIC/SOHIC/SCC)		Wet H2S Damage		Hydrogen Stress Corrosion HF
cracking Unit	High Temperature Hydrogen Attack		(Blistering/HIC/SOHIC/SCC)		Galvanic Corrosion
Onit	High Temperature H2/H2S Corrosion		Creep / Stress Rupture		Dissimilar Weld Metal (DMW) Cracking
	Polythionic Acid Stress Corrosion		Polythionic Acid Stress Corrosion	Hydrogen	High Temperature Hydrogen Attack
	Naphetanic Acid Corrosion		Naphetanic Acid Corrosion	Unit	(HŤHA)
	Creep / Stress Rupture		Ammonium Chloride Corrosion		Thermal Fatigue
	Temper Embrittlement		Thermal Fatigue		Temper Embittlement
	Ammonium Chloride Corrosion		Graphitization		Carbonate SCC
	Ammonium Bisulfide Corrosion		Temper Embrittlment		Amine Corrosion / Cracking
	Amine Corrosion / Cracking		Decarburization		Chloride SCC
	Hydrogen Embrittlement		Carburization		Thermal shock
	Chloride Stress Corrosion Cracking		Reheat Cracking		Reheat Cracking
	Brittle Fracture				CO ₂ Corrosion
	Reheat Cracking				Metal Dusting

Hydroprocessing reactors

Production of cleaner fuels in accordance with current standards requires a refinery to use hydrotreating units to reduce sulfur, aromatics, nitrogen, oxygen, and metals while improving the combustion quality and smoke point of naphtha, diesel, and kerosene.

Hydrotreating / hydrodesulphurization (HDS) reactors are critical equipment in a hydrotreating unit.

In order to increase the refinery's yield rate, however, conversion units are needed to crack the vacuum gas oil (VGO) and the atmospheric gas oil (AGO) as well as the gas oil from the coker and the visbreaker units. This method enables the refinery to process the residual oil ("the bottom-of-the-barrel"). For example, hydrocracking is a catalytic cracking process that is assisted by the presence of hydrogen. In this case, hydrocracking reactors are the critical equipment.

The common element among hydroprocessing reactors of this type is the use of advanced 2.25Cr-1Mo-0.25V material, which has numerous merits over conventional grade material, including greater tensile strength at elevated temperatures, enabling the industry to use reactors with lower wall thickness and weight (about 25% less weight). Additionally, it makes reactors less susceptible to damage mechanisms, such as temper embrittlement and high temperature hydrogen attack (HTHA) and last but not least, it provides stronger resistance to weld overlay disbonding induced by hot hydrogen.

Despite all these advantages, weld fabrication of reactors made of this grade of material ultimately becomes challenging due to various material sensitivities. e.g., weld cracking and re-heat cracking. Furthermore, intermediate and post-weld heat treatment as well as non-destructive examination (NDE) requires a different – and very precise – process compared to conventional 2.25Cr-1Mo grades. An example is the Time Of Flight Diffraction (TOFD) ultrasonic test.

Let's take a brief look at the welding of a hydroprocessing reactor:

A Fabrication of the reactor shell

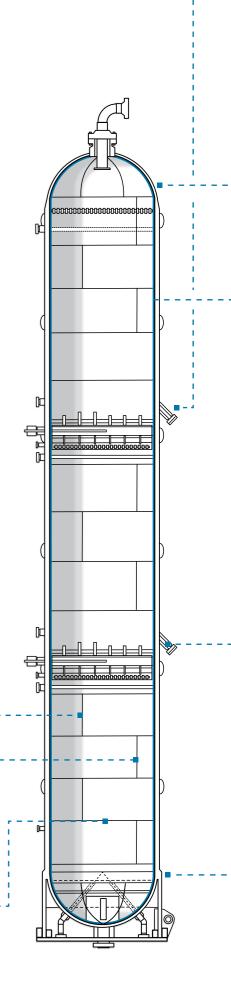
Depending on the design requirements and the wall thickness, shell material can be fabricated from plate or forged rings. If plates are used, they must be re-rolled and longitudinally welded to form a ring. A combination of both plate rings and forged rings is also possible, for example, forged rings for the quench zone and support skirt and plate rings for the rest of the shell arrangement.

Narrow gap submerged arc welding (SAW), either with tandem or single wire, is the process of choice. With our wire/flux combination and the corresponding parameter setting, it is feasible to have the smallest possible opening, which significantly reduces the consumption of filler metals and welding time.

A smaller amount of GTAW rod and SMAW electrode is also deposited.

Longitudinal Joints: ASME SA542 Gr. D CL 4a. ASME SA832 Gr. 22V

Circumferential Joints: Forged rings: ASME SA336 Gr. F22V Plate-fabricated rings: ASME SA832 Gr. 22V or ASME SA542 Gr. D, CL 4a



B Nozzle welds

Piping nozzles, instrumentation nozzles, as well as the hand holes are critical areas as they are the only openings of the reactor and must thereby withstand conditions within the reactor. The conventional method represents the use of the SMAW process for the nozzle welds, but experienced fabricators currently use single-wire SAW. Due to the especially restrained condition of the joint, ISR (intermediate stress relieving) is of paramount importance.

c Shell to dished end / dished end to support welds

Heads are either single-piece or multi-piece welded. Precise joint alignment is also needed as the dished end has a lower wall thickness compared to the shell. If forged profiles are used, skirt to bottom is sometimes a single forged piece.

D Weld overlay

The usual overlay deposit for such reactors is S.S 347. Depending on the accessibility and the cladding area, different processes are chosen:

Inside reactor: Strip cladding SAW, ESW 2 layer, ESW single layer, ESW high speed Inside nozzles, fittings and restoration: FCAW, SMAW, GTAW Weld-overlay build-up of the internal "supports": SMAW, GTAW. CrMo-22V FCAW 347

An important point to Cr-Mo 22V build up overlay is the necessity of ISR (intermediate stress relieving) due to restrained condition.

E Heat treatment

DHT: Dehydrogenation heat treatment of 350° C for 4 hours is essential to minimize the susceptibility to cold cracking due to residual hydrogen in the weld.

ISR: Intermediate stress relieving is necessary, especially for highly restrained joints such as nozzle welds. The recommended temperature for ISR is 650 – 670° C for 4 hours to ensure a partial elimination of the residual stresses in the weld.

PWHT: Post weld heat treatment for CrMo-22V has a very narrow tolerance in comparison to conventional steel grades. The recommended PWHT is 705° C for 8 hours.

Max PWHT: Several heat treatments are applied during fabrication, including DHT, ISR, and final PWHT. Sometimes, repairs are undertaken during fabrication. An additional cycle should be planned for any necessary repairs after installation. A maximum PWHT condition, which has an equal effect of all previously cited PWHT cycles, must be simulated. To that end, and to define one PWHT condition that covers all cycles, the Hollomon parameter (HP) of all the PWHTs should be calculated and then for any given time a PWHT temperature can be calculated vice versa.

 $\begin{aligned} \mathbf{HP} &= (273^{\circ}\text{C} + \mathbf{T}) \ge (20 + \log_{10}(\mathbf{t}/60)) \ 10^{-3} \\ \mathbf{T} &= 10^{3} \ \mathbf{HP}/(20 + \log_{10}(\mathbf{t}/60)) - 273^{\circ}\text{C} \\ \mathbf{t} &= 60 \ge 10^{(1000 \ \text{HP}/(273^{\circ}\text{C} + \mathbf{T}) - 20)} \end{aligned}$

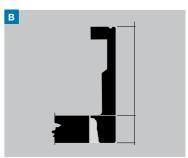
Step cooling: is done to simulate an accelerated embrittlement for evaluation of potential temper embrittlement.

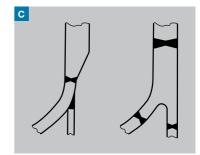
F Reheat cracking and tramp elements

Since introduction of this material, the industry has encountered many difficulties due to reheat cracking after PWHT. With precisely controlled amount of the tramp elements (Typical X factor: 8 and typical K factor: 0.7), the reheat cracking problem is under control.







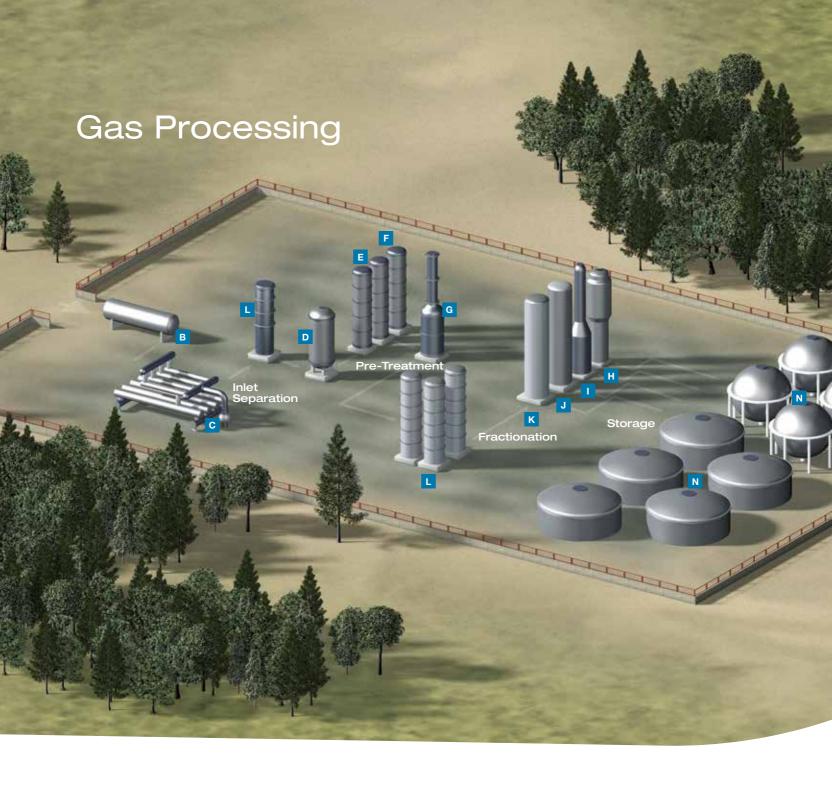






G Standard codes; recommended practices

ASME BPVC Section VIII Division 2, API RP 934A, API RP582, ASTM G146-01



In the form it is extracted, natural gas cannot be used as fuel or feedstock. It needs to be treated in gas processing plants. Irrespective of whether a gas processing plant is constructed for a specific gas field or inside a refinery to process refinery gases, it generally contains:

Inlet facilities:	To separate natural gas from water and impurities. These facilities can also include slug catcher manifold/drum
Pre-treatment:	To remove sulfur, $\rm H_{2}O, \rm Hg, \rm and \rm CO_{2}$ from natural gas
Fractionation:	To fractionate different gaseous and NGL hydrocarbons

The global gas resource landscape has changed significantly within the past decade. Unconventional gas, so called either due to its quality (sour and ultra-sour gas) or its source (shale gas, coal gas), has begun to play an important role. As such, there is a need for different solid or weld overlaid corrosion resistance alloys in different separators and fractionators. Examples are the injection lines, inlet separators, and slug catcher manifold / drums in which – depending on the sourness of the gas – S.S 316L, Alloy 825, or Alloy 625 weld overlay is applied.

Selection of the base material can also vary depending on the operating pressure or job site temperature. Use of carbon steel as well as low alloy / chrome-molly alloys is possible depending on the operating conditions.



In Table D, we have listed some of the critical process equipment in a gas processing plant. A number of the major damage mechanisms in a typical gas processing plant are listed in Table C. Some of these damage mechanisms can be controlled by selecting high-quality base material and welding consumables.

Unit	Damage Mechanism
Inlet Facilities	Wet H2S Blistering
	Wet H2S HIC
	Wet H2S SOHIC
	Wet H2S SCC
	Slugging
	Amine Degradation Corrosion
Pre-Treatment	Sulfidation
	Wet H2S damage (Blistering/HIC/SOHIC/SCC)
	Ammonium Bisulfide
	Alkaline SCC
	Erosion / Erosion-Corrosion
	Amine Cracking
	Amine Corrosion
	CO ₂ Corrosion
	Chloride Stress Corrosion Cracking
	Titanium Hybriding
	Sulfuric Acid
	Mercury Attack Corrosion
	Flue Gas Dew Point Corrosion

Table C: Damage mechanisms

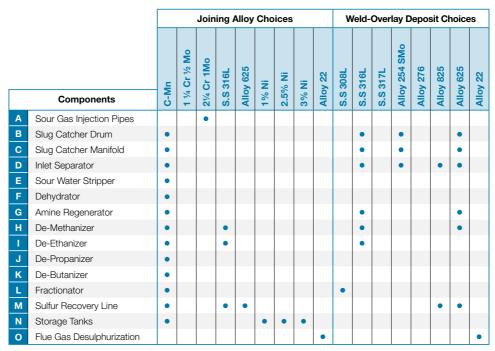


Table D: Alloy choices for main gas processing components

Olefins and Aromatics

Olefins (such as Ethylene and Propylene) and Aromatics (Benzene, Toluene, and Xylene) are key products in the petrochemical industry. Naphtha from the oil refinery enters the cracking furnace and is cracked by being heated to 1,150°C. The cracked hydrocarbon enters the quench oil / water columns. The gases are then compressed and liquefied in different temperatures down to -150°C.

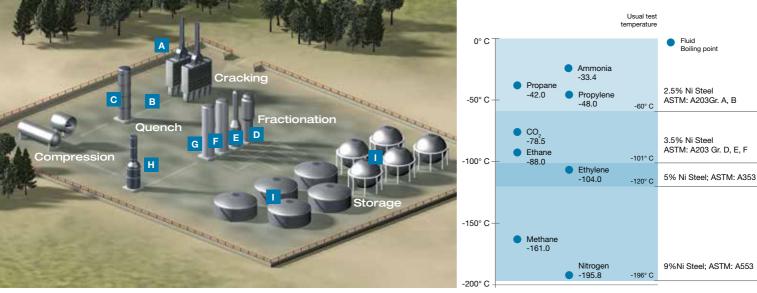


Table E: Steel choices for cryogenic application

A cracker furnace represents the heart of a plant (a description follows on the next page). voestalpine Böhler Welding draws upon many years of experience in the production of filler metals for welding the cracker furnace tubes. A plant has both high-temperature parts and lowtemperature areas. Various hydocarbons have very low boiling temperatures and therefore, low-temperature steels grades are needed for transport and storage of these materials within the plant. Some cryogenic products are listed in the products table of this brochure. However, all the LPG- and LNG-related products are separately described in our LNG/LPG brochure.

In Table F, we have listed some of the critical process equipment in an Olefin / Aromatic plant. A number of the major damage mechanisms from typical olefins/aromatics are listed in Table G. Some of these damage mechanisms can be controlled by selecting high-quality base material and welding consumables.

		Joining Alloy Choices											Weld-Over- lay Deposit Choices		
		C-Mn	Alloy 35 / 45 Nb	5Cr ½Mo	9Cr 1Mo	316L	347	310	S.S304H	Ni	% Ni	N	308L	316L	Alloy 625
	Components		Allo	5Cr	9Cr	S.S	S.S	S.S	S.S	1% Ni	2.5%	3%	S.S	S.S	Allo
Α	Cracking Furnace		•												
В	Post Furnace Piping			•	•		•	•	•						
С	Quench Column	•											•	•	
D	De-Methanizer	•				•								•	•
Е	De-Ethanizer	•				•								•	•
F	De-Propanizer	•													
G	De-Butanizer	•													
Н	Ethylene Oxide Reactor	•													
I.	Storage Tanks									•	•	•			

Table F: Alloy choices for main olefin/aromatic plant components

Unit	Damage Mechanism							
Cracking	Creep / Stress Rupture							
	Carburization							
	Temper Embrittlement							
	Thermal Shock							
	Graphitization							
	Thermal Fatigue							
	Caustic Corrosion							
	Caustic Crack							
Quench	Caustic Corrosion							
Fractionation	Caustic Crack							
	Low Temperature Embrittlement							

Table G: Damage mechanisms

Welding of Reformer and Cracker Tubes

In petroleum refining, there is the demand for a steam / catalytic reforming process that reforms the hydrocarbon molecule to a desired shape. This process is also used for hydrogen production in the hydrogen unit of large-scale refineries, where very large amounts of process hydrogen are needed. The operating temperature can exceed 900°C.

In petrochemical plants, e.g., in Olefin and Aromatic plants, naphtha from the refinery first enters into a cracker, the heart of the plant. The temperature in the cracker furnace can exceed 1,150°C. The cracking process leaves coke on the tube walls, which results in higher temperatures that can reach the operational limits.

In both of the above-mentioned applications, centrifugally cast tubes represent the main element of the process. The tubes and the respective welded joints must be able to withstand numerous damage mechanisms, including but not limited to creep / stress rupture, carburization, and fatigue. Being able to balance increased strength, higher creep resistance, and greater toughness has been a challenge for the industry. Over decades, the industry has benefited from the introduction of new alloys with various Cr and Ni content and the addition of alloying elements, such as Si, Ti, Zr, Nb, Mo, Co, etc. to create the ability to withstand higher operating temperatures and, at the same time, to reach reasonable creep strength and carburization resistance. Over-alloyed welding consumables have always been available in our portfolio, but similar or matching consumables for every new tube grade have been what we offer in order to minimize the difference between the thermal expansion coefficient in the weld joint and the tube; this enables a longer life cycle of the welded tubing. A list of the main products for the welding of furnace tubes is provided in the product section of this brochure.

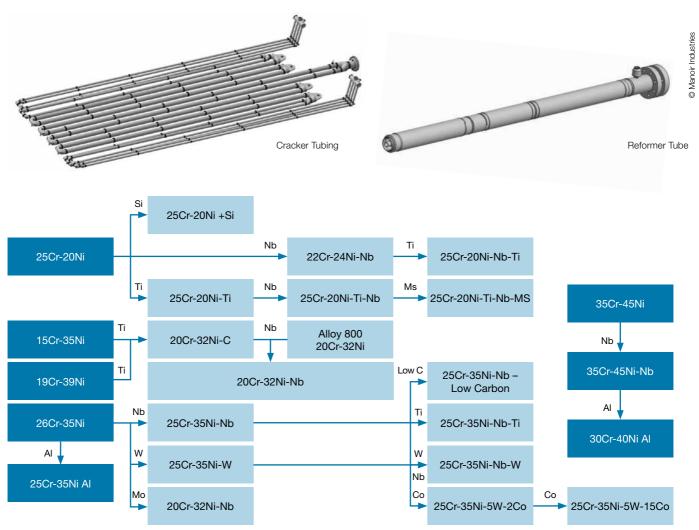
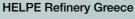


Table H: Cast tube alloy evolution

References





Fabricator name: Component: Base material: Joining products: Larsen and Toubro Hydrocracking Reactor (970 MT) CrMo-22V (292mm) SMAW: Phoenix Chromo 2V GTAW: Union I CrMo 2V SAW wire: Union S1 CrMo 2V SAW Flux: UV 430 TTR-W



Burgas Refinery Bulgaria

•	•						
Fabricator name:	Belleli Energy CPE S.r.L						
Component:	Hydroprocessing Reactors						
Base material:	CrMo-22V + S.S 347 (240 + 3mm)						
Joining products:	SMAW: Phoenix Chromo 2V						
	GTAW: Union I CrMo 2V						
	SAW wire: Union S1 CrMo 2V						
	SAW Flux: UV 430 TTR-W						
Cladding Products:	Strip: SOUDOTAPE 21.11 LNb, Flux: RECORD EST 122						



Mina Abduallah and Mina Al-Ahmadi Refinery Kuwait

Fabricator name: Larsen and Toubro Component: 22 Hydroprocessing Reactors Base material: CrMo 22, CrMo-22V Joining products: SMAW: Phoenix SH Chromo 2 KS, Phoenix Chromo 2V GTAW: Union I CrMo 910 Spezial, Union I CrMo 2V SAW wire: Union S1 CrMo 2, Union S1 CrMo 2V SAW Flux: UV 420 TTR-W, UV 430 TTR-W

This is a short list of some of our partners:

ATB Riva Calzoni SpA
Axens
Bechtel
Belleli Energy C.P.E S.r.I
Borsig GmbH
CB&I Lummus
Cessco Fabrication and Engineering
Chevron
Chiyoda
CNPC
Daelim
Doncaster Paralloy Ltd.
Doosan Engineering and Construction
Duralloy Technologies

ExxonMobil FBM Hudson Italiana Felguera Calereria Pesada Fluor Foster Wheeler GE - Nuovo Pignone General Welding Wroks Inc. Godrej and Boyce Haldor Topsoe Hitachi Zosen Hyundai Heavy Industries ISGEC Japan Steel Works KBR

- Koch Industries Kubota Metal Corporation Larsen and Toubro Lurgi MAN DWE GmbH Manoir Industries Officine Luigi Resta S.p.A **OLMI** OMZ PETROBRAS **Relliance Industries** Rolle S.p.A Samsung Engineering Schmidt + Clemens GmbH
- Schwartz Houtmont Shanghai Boiler Works Shell Global Solutions SINOPEC **Taylor Forge Engineering Products** Technip Tecnicas Reunidas **TOTAL Raffinage** Thyssenkrupp Uhde UOP V.R.V Winkels Worley Parsons

If the product list is missing, please contact us.

The industry experts of voestalpine Böhler Welding possess a deep technical understanding of industryspecific welding applications and processes. They have profound industry-related project expertise and are ready to discuss welding challenges with customers.

Please contact our Global Industry Segment Manager:

T. +39 02 39017 236 F. +39 02 39017 246 E. welding.chemical@voestalpine.com www.voestalpine.com/welding

The information and product properties contained in this printed material are non-binding and serve the exclusive purpose of technical orientation. They do not replace individual consultation provided by our sales and customer service teams. The information and product properties contained in this brochure are guaranteed only when specifically and contractually stipulated. Not responsible for printing errors or technical changes. Duplication in part or in whole is subject to explicit written permission by voestalpine Böhler Welding GmbH.

Joining 1/4

	Alloy Group	Base Material Examples	Welding Process	Product Name	Classification AWS/EN
	C-Mn	Plate: ASME SA516 GR. 55	SMAW	BÖHLER FOX EV 47	AWS A5.1: E7016-1H4R
		Plate: ASME SA516 GR. 60			EN ISO 2560-A: E 38 4 B 42 H5
		Plate: ASME SA516 GR. 65		BÖHLER FOX EV 50	EN ISO 2560-A: E 42 5 B 42 H5
		Plate: ASME SA516 GR. 70			AWS A5.1: E7018-1H4R
		Forged: ASME SA181 Gr. F1	SAW Wire	Union S 2 Si	AWS A5.17 EM12K
		Pipe: ASME SA105 Gr. A, B, C			EN ISO 14171 S2Si
		Pipe: ASME SA106 Gr. A, B, C	SAW Flux	UV 418 TT	
		Tube: ASME SA210 Gr. A, B, C	o, w hax		EN ISO 14174 SA FB 1 55 AC H5
			SAW Wire+Flux	Union S 2 Si + UV 418 TT	AWS A5.17-SFA 5.17 F7A6-EM12K
					EN ISO 14171-S 42 5 FB S2Si
s			SAW Wire	Union S 3 Si + UV	AWS A5.17 EH12K
teel				418 TT	EN ISO 14171 S3Si
d S			SAW Flux	UV 418 TT	-
oye					EN Iso 14174 SA FB 1 55 AC H5
Unalloyed Steels			SAW Wire+Flux	Union S 3 Si + UV 418 TT	AWS A5.17-SFA 5.17 F7A8-EH12K
					EN ISO 14171-S 46 6 FB S3Si
			GTAW	BÖHLER EMK 6	AWS A5.18: ER70S-6
					EN ISO 636-A: W 42 5 W3Si1
				BÖHLER EML 5	AWS A5.18 ER70S-3
					EN ISO 636-A: W 46 5 W2Si
			GMAW	BÖHLER EMK 6	AWS A5.18: ER70S-6
					EN ISO 14341-A: G3Si1 (wire)/ G 42 4 M21 3Si1
			FCAW	BÖHLER TI 52-FD	AWS A5.36: E71T-1M21A4-CS1-H8 E71T-1- C1A2-CS1-H4
					EN ISO 17632-A: T 46 4 P M 1 H10
					EN ISO 17632-A T 42 2 P C 1 H5
	C- ½ Mo	Plate: ASME SA571 Gr. J	SMAW	BÖHLER FOX	AWS A5.5: E7018-A1H4R
		Fitting: ASME SA 234 WP1, WP1		DMO Kb	EN ISO 2560-A: E Mo B B 42 H5
		Forging: ASME SA336 Gr. F1	SAW Wire	Union S 2 Mo	AWS A5.23 EA2
		Forged Fitting: ASME SA 182 Gr. F1			EN ISO 14171 S2Mo / EN ISO 24598-A S S Mo
		Pipe: ASME SA 335 Gr. P1	SAW Flux	UV 418 TT	-
		Tube: ASME SA 250 Gr. T1a, T1b			EN ISO 14174 SA FB 1 55 AC H5
		Tube: ASME SA209 Gr. T1	SAW Wire+Flux	Union S 2 Mo + UV	AWS A5.23-SFA 5.23 F8A6-EA2-A2
		Tube: EN10216-2: 16Mo3		418 TT	EN ISO 14171 S46 4 FB S2Mo
			GTAW	BÖHLER DMO-IG	AWS A5.28: ER70S-A1 (ER80S-G)
					EN ISO 21952-A: W Mo Si
ú			GMAW	BÖHLER DMO-IG	AWS A5.28: ER70S-A1 (ER80S-G)
ee					EN ISO 21952-A: G Mo Si
N.			FCAW	BÖHLER DMO TI-FD	AWS A5.36: E81T1-M21PY-A1H8
SSE					EN ISO 17634-A: T MoL P M 1 H10
e ≮	1 ¼ Cr ½ Mo	Plate: ASME SA387 Gr. 11 Gr. 12	SMAW	Phoenix Chromo 1	AWS A5.5 E8018-B2
uns	1 Cr ½ Mo	Fitting: ASME SA 234 WP11, WP12			EN ISO 3580-A ECrMo1 B 4 2 H5
res		Forging: ASME SA336 Gr. F11	SAW Wire	Union S 2 CrMo	AWS A5.23 EB2R
Low-alloyed Pressure Vessel Steels		Forged Fitting: ASME SA 182 Gr. F11, F12			EN ISO 24598-A S S CrMo1
allc					
Ň		Pipe: ASME SA 335, P11, P12	SAW Flux	UV 420 TTR	
		Tube: ASME SA 213 T11, T12			EN ISO 14174 SA FB 1 65 DC
				UV 420 TTR-W	
					EN ISO 14174 SA FB 1 65 AC
			SAW Wire+Flux	Union S 2 CrMo + UV 420 TTR(-W)	AWS A5.23-SFA 5.23 F8P2-EB2R-B2
					EN ISO 24598-A S S CrMo1 FB
			GTAW	Union I CrMo	AWS A5.28 ER80S-G [ER80S-B2 (mod.)]
					EN ISO 21952-A W CrMo1Si EN ISO 21952-B W 55 1CM3
				Union ER 80S-B2	AWS A5.28 ER80S-B2





Joining 2/4

	Alloy Group	Base Material Examples	Welding Process	Product Name	Classification AWS/EN
	0.1/ 0×1 Ма	Plate: ASME SA387 Gr. 22	SMAW	Phoenix SH	AWS A5.5 E9015-B3
	2 ¼ Cr 1 Mo	Plate: ASME SA387 Gr. 22	SIMAW	Chromo 2 KS	AWS A5.5 E9015-B3
		Fitting: ASME SA 234 WP22			EN ISO 3580-A ECrMo2 B 4 2 H5 EN ISO 3580-B E 6215-2C1M
		Forging: ASME SA336 Gr. F22	SAW Wire	Union S 1 CrMo 2	AWS A5.23 EB3R
		Forged Fitting: ASME SA 182 Gr. F22			EN ISO 24598-A S S CrMo2
		Pipe: ASME SA 335, P22	SAW Flux	UV 420 TTR	-
		Tube: ASME SA213 Gr. T22			EN ISO 14174 SA FB 1 65 DC
s				UV 420 TTR-W	-
Stee					EN ISO 14174 SA FB 1 65 AC
essel			SAW Wire+Flux	Union S1 CrMo 2 + UV 420 TTR(-W)	AWS A5.23-SFA 5.23 F9P2-EB3R-B3R
Low-alloyed Pressure Vessel Steels			GTAW	Union I CrMo 910 Spezial	AWS A5.28 ER90S-G
Pre				Union ER 90S-B3	AWS A5.28 ER90S-B3
ved					EN ISO 21952-B W 2C1M
allo	2 ¼ Cr 1 Mo ¼ V	Plate: ASME SA542 Type D, CL 4a	SMAW	Phoenix Chromo 2V	AWS A5.5 E9015-G
-×o		Plate: ASME SA832 Gr. 22V			EN ISO 3580-A E ZCrMoV2 B 4 2 H5
		Forging: ASME SA336 Gr. F22V, SA541 Gr. 22V	SAW Wire	Union S 1 CrMo 2V	AWS A5.23 EG
		Forged Fitting: ASME SA 182 Gr. F22V			EN ISO 24598-A S S Z CrMoV2
			SAW Flux	UV 430 TTR-W	-
					EN ISO 14174 SA FB 1 57 AC
			SAW Wire+Flux	Union S1 CrMo 2V + UV 430 TTR-W	AWS A5.23 F9PZ-EG-G
					EN ISO 24598-A S S Z CrMo 2V FB
			GTAW	Union I CrMo 2V	AWS A5.28 ER90S-G
	5 Cr ½ Mo	Plate: ASME SA387 Gr. 5 CL.	SMAW	BÖHLER FOX CM 5 Kb	AWS A5.5: E8018-B6H4R
s		Fitting: ASME SA 234 WP5 Forging: ASME SA336 Gr. F5	SAW Wire	Union S1 CrMo 5	EN ISO 3580-A: ECrMo5 B 4 2 H5 AWS A5.23 EB6
teel		Forged Fitting: ASME SA 182 Gr. F5	SAW WIE		EN ISO 24598-A S S CrMo5
e S		Pipe: ASME SA335 Gr. P5	SAW Flux	UV 420 TT	-
ratu		Tube: ASME SA213 Gr. T5			EN ISO 14174 SA FB 1 65 AC
High Temperature Steels			GTAW	BÖHLER CM 5-IG	AWS A5.28: ER80S-B6
Ē					EN ISO 21952-A: W CrMo5Si
Higl			GMAW	BÖHLER CM 5-IG	AWS A5.28: ER80S-B6
/ed					EN ISO 21952-A: G CrMo5Si
Medium-alloye	9 Cr 1 Mo	Plate: ASME SA387 Gr. 9	SMAW	BÖHLER FOX CM 9 Kb	AWS A5.5: E8018-B8
Ę		Fitting: ASME SA234 WP9 Forging: ASME SA336 Gr. F9			EN ISO 3580-A: ECrMo9 B 4 2 H5
ledi		Forged Fitting: ASME SA 182 Gr. F9			
2		Pipe: ASME SA335 Gr. P9	GTAW	BÖHLER CM 9-IG	AWS A5.28 ER80S-B8
		Tube: ASME SA213 Gr. T9			EN ISO 21952-A G CrMo9Si
	S.S 304H	UNS30409	SMAW	Thermanit ATS 4	AWS A5.4 E308H-15
					EN ISO 3581-A E 19 9 H B 2 2
			SAW Wire	Thermanit ATS 4	AWS A5.9 ER19-10H
eels					EN ISO 14343 S 19 9 H
ss St			SAW Flux	Marathon 104	EN ISO 14174 SA FB 2 55 AC H5
inles				Thormonit ATS 4	
Sta			SAW Wire+Flux	Thermanit ATS 4 + Marathon 104	AWS A5.9 ER19-10H
tant					EN ISO 14343 S 19 9 H
sist			GTAW	Thermanit ATS 4	AWS A5.9 ER19-10H
Heat Resistant Stainless Steels					EN ISO 14343-A W 19 9 H / EN ISO 14343-B SS19-10H
т			GMAW	Thermanit ATS 4	AWS A5.9 ER19-10 H
					EN ISO 14343-A G 19 9 H /
					EN ISO 14343-B SS19-10H



Joining 3/4

	Alloy Group	Base Material Examples	Welding Process	Product Name	Classification AWS/EN
<u>0</u>	S.S 304H	UNS30409	FCAW	BÖHLER E 308 H	AWS A5.22: E308HT1-1/4
Heat Resistant Stainless Steels	5.5 504H	011330409	FCAW	PW-FD Bi-Free	AWS A5.22. E306H11-1/4
ss					EN 17633-A: T Z 19 9 H P C1/M21 1
linle	S.S 310	UNS31000	SMAW	Thermanit C	AWS A5.4 E310-15 (mod.)
Ste				The sum and the O	EN ISO 3581-A E25 20 B 2 2
tant			GTAW	Thermanit C Si	AWS A5.9 ER310 (mod.)
esis					EN ISO 14343-A W 25 20 Mn / EN ISO 14343-B SSZ31
atR			GMAW	Thermanit C Si	AWS A5.9 ER310 (mod.)
Ре					EN ISO 14343-A G 25 20 Mn
	Wrought:		SMAW	UTP 2133 Mn	-
	Alloy 800	UNS8800			EN ISO 3581-A: EZ 21 33 B 4 2
	Alloy 800H	UNS8810	GTAW	UTP A 2133 Mn	-
	Alloy 800HT	UNS8811			EN ISO 14343: WZ 21 33 Mn Nb
/ed			GMAW	UTP A 2133 Mn	-
alloy	Cast Tubes:		SMAW	UTP 2535 Nb	EN ISO 14343: GZ 21 33 Mn Nb
gh-:	Alloy HK		GWAW	011 2303 105	EN 1600: EZ 25 35 Nb B 6 2
θH	Alloy HP		GTAW	UTP A 2535 Nb	-
atur	Alloy HP Nb				EN ISO 14343-A: WZ 25 35 Zr
High Temperature High-alloyed	Alloy HP M.A		GMAW	UTP A 2535 Nb	-
Ten					EN ISO 14343-A: GZ 25 35 Zr
ligh	Cast Tubes	GX45NiCrNbSiTi 45-35	SMAW	UTP 3545 Nb	-
-	Alloy 35/45		GTAW	UTP A 3545 Nb	EN 1600: EZ 35 45 Nb B 6 2
	Alloy 35/45 M.A		GTAW	UTP A 3545 ND	- EN ISO 14343-A: WZ 35 45 Nb
			GMAW	UTP A 3545 Nb	-
					EN ISO 14343-A: GZ 35 45 Nb
	Austanitia	C C 2001	SMAW	BÖHLER FOX CN	
	Austenitic	S.S 309L	SIVIAVV	23/12	AWS A5.4: E309L-17
		Only Weld-Overlay Buffer			EN ISO 3581-A: E 23 12 L R 3 2
			SAW Wire	Thermanit 25/14 E309L	AWS A5.9 ER309L
				ESUAL	EN ISO 14343 S 23 12 L
			SAW Flux	Marathon 431	
					EN ISO 14174 SA FB 2 64 DC
			GTAW	BÖHLER CN 23/12-IG	AWS A5.9: ER309L
					EN ISO 13343-A: G 23 12 L
			GMAW	Thermanit 25/14	AWS A5.9 ER 309 L Si
				E309L Si	
			FCANA	BÖHLER CN 23/12-FD	EN ISO 14343-A G 23 12 L Si
teel			FCAW	BUHLER CN 23/12-FD	AWS A5.22: E309LT0-4/1 EN 17633-A: T 23 12 L R M21 (C1) 3
Stainless Steel	Austenitic	S.S 321/347	SMAW	BÖHLER FOX SAS 2	
linle	Nb Stabilized		_		EN ISO 3581-A: E 19 9 Nb B 2 2
Sta			SAW Wire	Thermanit H-347	AWS A5.9 ER347
					EN ISO 14343 S 19 9 Nb
			SAW Flux	Marathon 431	
			OTAVA		EN ISO 14174 SA FB 2 64 DC
			GTAW	BÖHLER SAS 2-IG	AWS A5.9: ER347 EN ISO 13343-A: W 19 9 Nb
			GMAW	Thermanit H-347	AWS A5.9 ER 347
					EN ISO 14343-A G 19 9 Nb /
					EN ISO 14343-B SS347
				Thermanit H Si	AWS A5.9 ER 347Si
					EN ISO 14343-A G 19 9 Nb Si /
					EN ISO 14343-B SS347Si
			FCAW	BÖHLER SAS 2-FD	EN ISO 17633-A: T 19 9 Nb R M21/C1 3
					AWS A5.22: E347T0-4/1

Joining 4/4

	Alloy Group	Base Material Examples	Welding Process	Product Name	Classification AWS/EN
	Alloy 600	UNSN06600	SMAW	UTP 068 HH	AWS A5.11 : E NiCrFe-3 (mod.)
					EN ISO 14172 : E Ni 6082 (NiCr20Mn3Nb)
			GTAW	UTP A 068 HH	AWS A5.14 : ER NiCr-3
					EN ISO 18274 : S Ni 6082 (NiCr20Mn3Nb)
			GMAW	UTP A 068 HH	AWS A5.14 : ER NiCr-4
					EN ISO 18274 : S Ni 6082 (NiCr20Mn3Nb)
	Alloy 625	UNS06625	SMAW	UTP 6222 Mo	AWS A5.11 : E NiCrMo-3
ø	Alloy 825	UNS08825			EN ISO 14172 : E Ni 6625 (NiCr22Mo9Nb)
Nickel-base			GTAW	UTP A 6222 Mo	AWS A5.14 : ER NiCrMo-3
kel					EN ISO 18274 : S Ni 6625 (NiCr22Mo9Nb)
Nic			GMAW	UTP A 6222 Mo	AWS A5.14 : ER NiCrMo-4
					EN ISO 18274 : S Ni 6625 (NiCr22Mo9Nb)
	Alloy 617	UNS06617	SMAW	UTP 6170 Co	AWS A5.11 : ~ ENiCrCoMo-1 (mod.)
					EN ISO 14172 : ~ E Ni 6117~ (NiCr22Co12Mo)
			GTAW	UTP A 6170 Co	AWS A5.14 : ER NiCrCoMo-1
					EN ISO 18274 : S Ni 6617 (NiCr22Co12Mo9)
			GMAW	UTP A 6170 Co	AWS A5.14 : ER NiCrCoMo-2
					EN ISO 18274 : S Ni 6617 (NiCr22Co12Mo9)
	1% Ni	ASME SA572 Gr. 65	SMAW	BÖHLER FOX EV 60	AWS A5.5 E8018-C3H4R
		ASME SA573			EN ISO 2560-A E 46 6 1Ni B 42 H5
			SAW Wire	Union S 3 NiMo 1	AWS A5.23 EF3
					EN ISO 14171 S3NiMo1
			SAW Flux	UV 420 TT(R)	-
				-	EN ISO 14174 SA FB 1 65 DC
			GTAW	BÖHLER Ni1-IG	AWS A5.28 ER80S-Ni1 (mod.)
					EN ISO 636-A W3Ni
			GMAW	BÖHLER NiMo1-IG	AWS A5.28 ER90S-G
					EN ISO 16834-A G Mn3Ni1Mo (wire) / G 55 6 M21 Mn3Ni1Mo
	2-2.5% Ni	ASME SA203 Gr. A & B ASME SA572 Gr. 65	SMAW	BÖHLER FOX 2,5 Ni	AWS A5.5 E8018-C1H4R EN ISO 2560-A E 46 8 2Ni B 42 H5
			SAW Wire	Union S 2 Ni 2,5	AWS A5.23 ENi2
s					EN ISO 14171 S2Ni2
teel			SAW Flux	UV 418 TT, UV 421 TT	-
e S					EN ISO 14174 SA FB 1 55 AC H5
perature Steels			SAW Wire+Flux	Union S 2 Ni 2,5 + UV 418 TT	AWS A5.23-SFA 5.23 F8A10-ENi2-Ni2
em					EN ISO 14171 S 46 8 FB S2Ni2
Low-tem			GTAW	BÖHLER 2,5 Ni-IG	AWS A5.28 ER80S-Ni2
Ĕ					EN ISO 636-A W2Ni2 / W 46 8 W2Ni2
			GMAW	BÖHLER 2,5 Ni-IG	AWS A5.28 ER80S-Ni2 (wire) / G 46 8 M/C G2Ni2
					EN ISO 14341-A G2Ni2
	3.5% Ni	ASME SA203 Gr. D, E, F	SMAW	Phoenix SH Ni 2	AWS A5.5 E7018-C2L
				K 80	EN ISO 2560-A E 42 6 3Ni B 3 2 H5
			SAW Wire	Union S 2 Ni 3,5	AWS A5.23 ENi3
					EN 756 S2Ni3
			SAW Flux	UV 418 TT	- EN ISO 14174 SA FB 1 55 AC H5
			SAW Wire+Flux	Union S 2 Ni 3,5 + UV 418 TT	AWS A5.23-SFA 5.23 F8A15-ENi3-Ni3
					EN ISO 14171 S 46 8 FB S2Ni3
			GTAW	Union I 3,5 Ni	AWS A 5.23 ER80S-Ni3 (mod.)
					EN 1668 W Z42 10 W2Ni3



Strip Cladding

	Deposited Alloy	Welding Process	Layer	Strip	Flux
	S.S 410S	SAW	1st Layer	SOUDOTAPE 430	RECORD INT 101
		ESW	1st Layer	SOUDOTAPE 430	RECORD EST 122
	S.S 308L	SAW	1st Layer	SOUDOTAPE 309 L	RECORD INT 109
			2nd Layer	SOUDOTAPE 308 L	RECORD INT 109
		ESW	1st Layer	SOUDOTAPE 309 L	RECORD EST 122
			2nd Layer	SOUDOTAPE 308 L	RECORD EST 122
		ESW Single layer	Single Layer	SOUDOTAPE 308 L	RECORD EST 308-1
		ESW High Speed	1st Layer	SOUDOTAPE 309 L	RECORD EST 136
	S.S 308H	SAW	1st Layer	SOUDOTAPE 309 L	RECORD INT 101
			2nd Layer	SOUDOTAPE 308 L	RECORD EST 136
[S.S 316L	SAW	1st Layer	SOUDOTAPE 309 L	RECORD INT 109
			2nd Layer	SOUDOTAPE 316 L	RECORD INT 109
		ESW	1st Layer	SOUDOTAPE 309 L	RECORD EST 122
			2nd Layer	SOUDOTAPE 316 L	RECORD EST 122
ē		ESW Single layer	Single Layer	SOUDOTAPE 21.13.3 L	RECORD EST 122
Steinless Steel		ESW High Speed	1st Layer	SOUDOTAPE 309 L	RECORD EST 136
ess			2nd Layer	SOUDOTAPE 316 L	RECORD ESt 136
einl	S.S 317L	SAW	1st Layer	SOUDOTAPE 21.13.3 L	RECORD INT 101 Mo
ş			2nd Layer	SOUDOTAPE 316 L	RECORD INT 101 Mo
		ESW	1st Layer	SOUDOTAPE 316 L	RECORD EST 317-2
			2nd Layer	SOUDOTAPE 316 L	RECORD EST 317-2
		ESW Single layer	Single Layer	SOUDOTAPE 21.13.3 L	RECORD EST 317-1
	S.S 347	SAW	1st Layer	SOUDOTAPE 309 L	RECORD INT 109
			2nd Layer	SOUDOTAPE 347	RECORD INT 109
		ESW	1st Layer	SOUDOTAPE 309 L	RECORD EST 122
			2nd Layer	SOUDOTAPE 347	RECORD EST 122
		ESW Single layer	Single Layer	SOUDOTAPE 21.11 LNb	RECORD EST 122
		ESW High Speed	Single Layer	SOUDOTAPE 24.12 LNb	RECORD EST 136
		ESW High Speed	1st Layer	SOUDOTAPE 309 L	RECORD EST 136
			2nd Layer	SOUDOTAPE 347	RECORD EST 136
	Alloy 254 SMO	ESW	1st Layer	SOUDOTAPE 254SMo	RECORD EST 122
			2nd Layer	SOUDOTAPE 254SMo	RECORD EST 122
		ESW	1st Layer	SOUDOTAPE 309L	RECORD EST 122
	Alloy 276	ESW	1st Layer	SOUDOTAPE NiCrMo59	RECORD EST 259
			2nd Layer	SOUDOTAPE NiCrMo4	RECORD EST 259
	Alloy 59	ESW	1st Layer	SOUDOTAPE NiCrMo59	RECORD EST 259
			2nd Layer	SOUDOTAPE NiCrMo59	RECORD EST 259
	Alloy 825	ESW	1st Layer	SOUDOTAPE 825	RECORD EST 201
			2nd Layer	SOUDOTAPE 825	RECORD EST 201
		ESW Single layer	Single Layer	SOUDOTAPE 825	RECORD EST 138
	Alloy 625	SAW	1st Layer	SOUDOTAPE 625	RECORD NFT 201
			2nd Layer	SOUDOTAPE 625	RECORD NFT 201
		ESW	1st Layer	SOUDOTAPE 625	RECORD EST 201
			2nd Layer	SOUDOTAPE 625	RECORD EST 201
ø		ESW Single layer	Single Layer	SOUDOTAPE 625	RECORD EST 625-1
Bas		ESW High Speed	1st Layer	SOUDOTAPE 625	RECORD EST 236
ê			2nd Layer	SOUDOTAPE 625	RECORD EST 236
Nickel-Base	Alloy 400	SAW	1st Layer	SOUDOTAPE NiCu7	RECORD NiCuT
-			2nd Layer	SOUDOTAPE NiCu7	RECORD NiCuT
			3rd Layer	SOUDOTAPE NiCu7	RECORD NiCuT
		ESW	1st Layer	SOUDOTAPE NiCu7	RECORD EST 400
			2nd Layer	SOUDOTAPE NiCu7	RECORD EST 400
	Alloy 200	SAW	1st Layer	SOUDOTAPE NITI	RECORD NIT
			2nd Layer	SOUDOTAPE NITI	RECORD NIT
			3rd Layer	SOUDOTAPE NITI	RECORD NIT
		ESW	1st Layer	SOUDOTAPE NITI	RECORD EST 200
			2nd Layer	SOUDOTAPE NITI	RECORD EST 200
			Ord Lover	SOUDOTAPE NITI	RECORD EST 200
			3rd Layer	SOUDOTAFE NIT	TIEGOTIB EST 200
-	Alloy 22	ESW	1st Layer 2nd Layer	SOUDOTAPE NIT SOUDOTAPE NiCrMo22 SOUDOTAPE NiCrMo22	RECORD EST 259 RECORD EST 259

voestalpine Böhler Welding



voestalpine Böhler Welding

Böhler Welding know-how joins steel

Customers in over 120 countries join the expertise of voestalpine Böhler Welding (formerly the Böhler Welding Group). Focused on filler metals, voestalpine Böhler Welding offers extensive technical consultation and individual solutions for industrial welding and soldering applications. Customer proximity is guaranteed by 40 subsidiaries in 28 countries, with the support of 2,200 employees, and through more than 1,000 distribution partners worldwide.



fontargen brazing

Böhler Welding – More than 2,000 products for joint welding in all conventional arc welding processes are united in a product portfolio that is unique throughout the world. Creating lasting connections is the brand's philosophy in welding and between people.

UTP Maintenance – Decades of industry experience and application know-how in the areas of repair as well as wear and surface protection, combined with innovative and custom-tailored products, guarantee customers an increase in the productivity and protection of their components.

Fontargen Brazing – Through deep insight into processing methods and ways of application, Fontargen Brazing provides the best brazing and soldering solutions based on proven products with German technology. The expertise of this brand's application engineers has been formulated over many years of experience from countless application cases.

forwarded by:

Global Industry Segment Management Oil & Gas Downstream

T. +49 (0) 2381 271 441 F. +49 (0) 2381 271 479 E. welding.downstream@voestalpine.com



voestalpine Böhler Welding www.voestalpine.com/welding